

Incorporating the MSC1210 into Electronic Weight Scale Systems

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ABSTRACT

The MSC1210 is an integrated system for single-chip high-resolution measurements. Inside the device, there is a 24-bit $\Delta\Sigma$ (delta-sigma) analog core and an enhanced 8051 microprocessor. This application note discusses how the MSC1210 can be incorporated into an electronic weight scale system. It was found that the system had a display (count) resolution of 1 count in 62500 (with software averaging) using a 5kg capacity, 2mV/V Tedeo-Huntleigh TH1042 load cell. The internal resolution of the Analog-to-Digital converter was better than 1 count in 600000.

Contents

1	Load Cell Fundamentals.....	3
2	Weight Measurements Using a Load Cell and the MSC1210	4
3	Theory	5
	3.1 Decimation Ratio	5
	3.2 PGA and Buffer	6
	3.3 Offset and Gain Calibration of Load Cell.....	6
	3.4 Calculating the Display Resolution (Count).....	7
	3.5 Reference Voltage.....	8
	3.6 Filtering, Display Rate, and Settling Time	9
	3.7 Dynamically Controlled Window Sizes	9
	3.8 Temperature Drift Compensation	10
4	Results	11
	4.1 No Averaging.....	12
	4.2 Running Average.....	14
5	Summary.....	16
	Example Code	16
	References.....	22

Figures

Figure 1.	Schematic of TH1042 High Precision Load Cell.....	3
Figure 2.	Load Cell Setup	5
Figure 3.	Output Voltage vs. Load	7
Figure 4.	Example of State Machine for Dynamically Controlling Window Sizes	10
Figure 5.	200 Consecutive Readings	12
Figure 6.	Histogram for Data in Figure 5.....	13
Figure 7.	200 Consecutive Readings, Window Size = 8	14
Figure 8.	Histogram for Data in Figure 7.....	15

Tables

Table 1.	Bin Number and Interval	13
Table 2.	Bin Number and Interval	15
Table 3.	Summary of Results.....	15

1 Load Cell Fundamentals

Nearly every electronic weighing system uses load cells. These cells convert a force or weight into an electrical signal. A strain gauge is the heart of a load cell. The resistance of a strain gauge changes when it is stressed. Strain gauges are typically made from ultra-thin heat-treated metallic foil and chemically bonded to a thin dielectric layer, known as a gauge patch. These patches are then adhered to the surface of the strain element. As the surface becomes strained, the gauge stretches or compresses, changing its resistance in proportion to the applied load. One strain gauge forms one leg of the four-legged Wheatstone bridge. The other three legs have constant resistance. When the excitation voltage (difference between the IN pins) is applied to the circuit, the output (difference between the OUT pins) becomes a differential voltage that is proportional to the force on the cell.

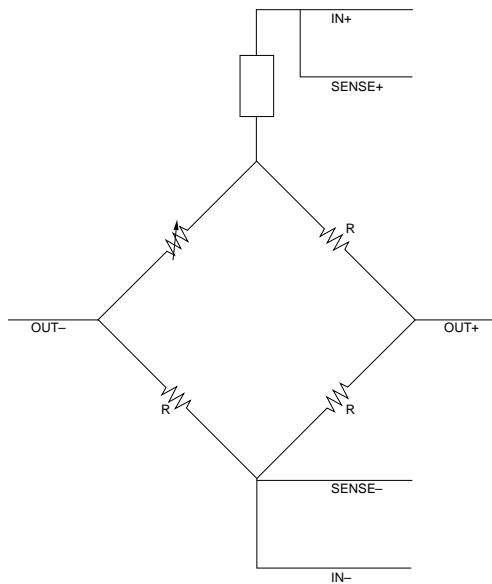


Figure 1. Schematic of TH1042 High Precision Load Cell

Most load cells are specified in terms of maximum capacity and output rating. Maximum capacity defines the maximum load (in kg) to which the load cell can be stressed. After this value is reached, the output voltage no longer changes. The output rating is given in mV/V. For example, a 2mV/V rating indicates that the full-scale output (at maximum capacity) is 10mV if the excitation voltage is 5V.

Since the differential output voltage varies in a linear relation to the weight applied, we can determine the weight from the output voltage ratiometrically. That is, we divide the observed output voltage by the rated output at the excitation voltage. For example, the observed output voltage is 1mV, the rated output is 2mV/V, the excitation voltage is 5V, and the capacity is 5kg; we can then calculate the measured mass (in kg):

$$\begin{aligned}
 \text{Mass (kg)} &= (\text{observed voltage (in volts)}) / (\text{voltage at capacity (in volts)}) * \text{capacity (in kg)} \\
 &= (\text{observed voltage}) / (\text{rated output} * \text{excitation}) * \text{capacity} \\
 &= 1\text{mV} / (2\text{mV/V} * 5\text{V}) * 5\text{kg} = 0.5\text{kg}
 \end{aligned}$$

2 Weight Measurements Using a Load Cell and the MSC1210

The primary goal of a weight measurement system is to convert the differential output signal from the load cell into a weight reading that can be displayed. The performance of a weight scale is based on its accuracy and display resolution (also known as count). Count is defined as the maximum number of bits on the display that are noise-free. To have a high count, we want the noise to be as small as possible. Display resolution (count) is key to determining the performance of a weight scale. A higher count is a strong indicator of better performance.

As a rule of thumb, to have a weight scale with a display resolution of 1 count in 60000, we need to use an analog-to-digital (A/D) converter having an internal resolution at least 4 times greater than the display resolution. That is, the internal resolution should be better than 1 count in 240000, or equivalently, the ADC must have an effective number of bits (ENOB) value of greater than 18.

In contemporary weight scale systems, multiple devices are needed:

- an A/D converter to convert the analog signal from the load cell output to a digital signal;
- an external reference source for the ADC;
- a microcontroller to process these digital signals (for example, convert to weight);
- peripherals to display weights and drivers to communicate with these peripherals;
- an excitation source to power the load cell.

In using the MSC1210, we replace the ADC, microcontroller, and drivers with a single chip. The only external components needed are the load cell, excitation source, external reference source (this should be ratiometric to the excitation source), and the display. Figure 2 shows how the MSC1210 is used in our weight scale application.

For excitation of the load cell, we use a 5V power supply. The internal reference is not used; instead, the power supply is also used as the ADC reference. A 10 μ F capacitor tied to ground is used to filter out the noise in the power supply. This pin is tied to input pin REF IN+ to provide the ADC with a reference. The pin REF IN- is grounded.

The outputs of the load cell (OUT+, OUT-) are filtered first to remove any noise that could have been generated in the load cell itself. We found that the arrangement shown here (Fig. 2) of two resistors and one capacitor provided the best results in terms of noise performance.

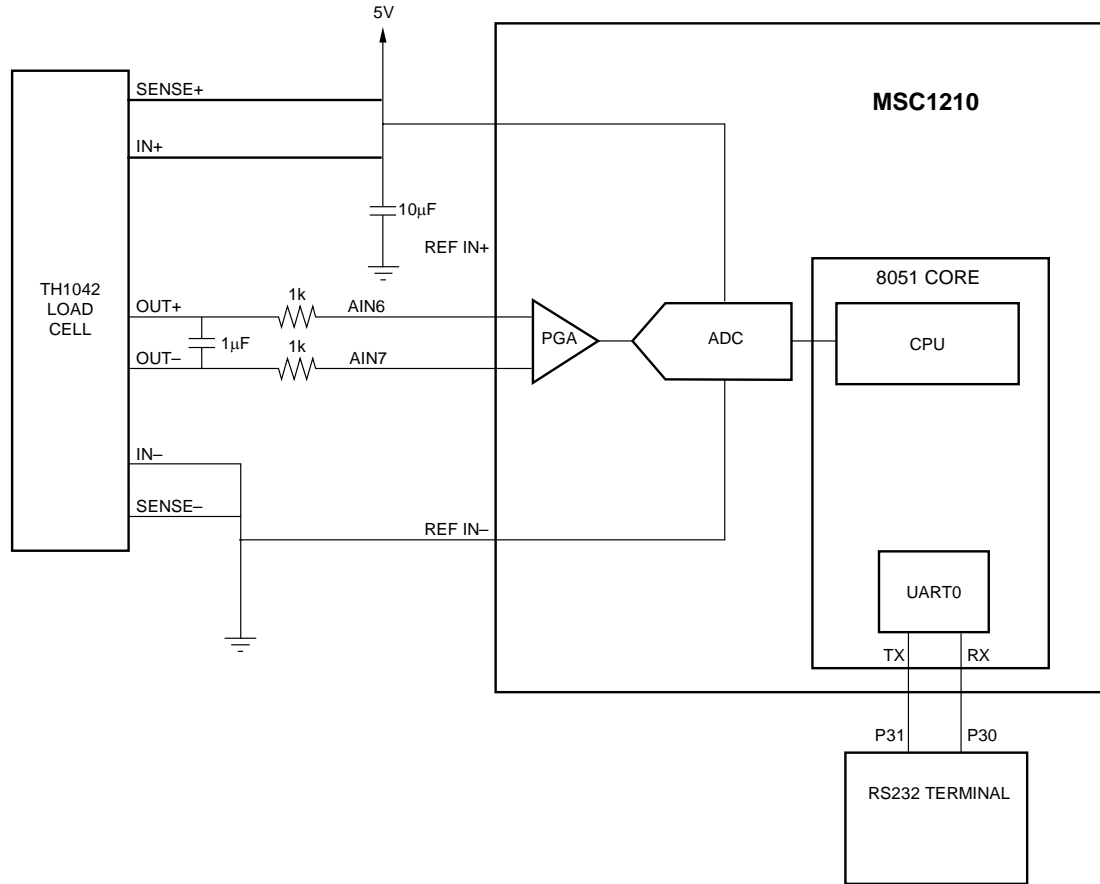


Figure 2. Load Cell Setup

3 Theory

3.1 Decimation Ratio

The ADC output data or acquisition rate is defined as:

$$\text{Data Rate} = \text{fmod} / (\text{Decimation Ratio})$$

$$\text{Where fmod} = (\text{External crystal frequency}) / ((\text{ACLK} + 1) * 64)$$

The external crystal frequency is 11.0592 MHz; thus, the ACLK register is set to 10. The decimation ratio is set to 1571 in order to get an ADC data output rate of 10Hz. That is, the ADC outputs a 24-bit number every 0.1s. The output rate of 10Hz is chosen because 60Hz is a multiple of 10Hz at which line frequency is a significant problem for low-level measurements. There also exists noise generated by the mechanical vibration of the load cell. This vibration is typically at a frequency of 20Hz. By setting the data rate to 10Hz, we effectively filter out any line frequency interference and mechanical noise from the load cell.

In countries where 50Hz is the standard line frequency, an output rate of 10Hz can also filter out any line interference. The highest output rate that can filter out the interference is 50Hz. To generate a rate of 50Hz, ACLK is set to 1 and the decimation ratio is set to 1728. Other ACLK and decimation ratio combinations exist that could generate a rate of 50Hz, but this is the setting for which the decimation ratio is highest. According to the datasheet, we can achieve a higher A/D effective number of bits (ENOB) at higher decimation ratios.

3.2 PGA and Buffer

PGA is set to 128 because we know the output rating of load cells is typically 2mV/V. For an excitation of 5V, there would be a maximum differential voltage on the order of 10mV across the output pins of the load cell. By amplifying this signal by a factor of 128, the maximum differential voltage is 1.28V. We therefore achieve smaller least-significant bit (LSB) resolution without saturating the ADC input. Here we assume the ADC reference is the same as the excitation voltage (reference voltages are discussed further on in this section). The LSB resolution in bipolar mode is defined as:

$$\text{LSB resolution} = \text{FSR}/2^{24}.$$

Where FSR is the full-scale range of the ADC.

$$\text{FSR} = (2 * \text{reference voltage}) / \text{PGA setting}$$

For a PGA of 1 and external reference = 5V, we have an FSR of 10V and LSB resolution of 600nV. For a PGA of 128, we have an FSR of 78.125mV and LSB resolution of 4.67nV. The buffer is off; according to the MSC1210 datasheet, we achieve better noise performance than when the buffer is on.

One drawback of amplifying the input signal is that the undesired noise is also amplified. Thus, the noise-performance is reduced at high PGA settings. According to the MSC1210 datasheet, we should expect an ENOB value of about 19 to 20 bits for a PGA setting of 128 and a decimation ratio of 1571. An ENOB of 19 to 20 (1 count in 1000000) is acceptable because this value is more than four times the display resolution (count).

3.3 Offset and Gain Calibration of Load Cell

Typical load cells have rated outputs of about 2mV/V. To find an exact and accurate rated output value for this particular load cell, we need to measure the differential output when a load of known weight is applied to it. These points are then plotted on a graph and curve fitting is performed in order to find a best-fit curve or line through those points. First, we have to measure the zero offset output voltage of the load cell; that is, the differential output when no load is applied. Known weights are applied to the load cell and the output voltages are then recorded. The zero offset is subtracted from these weight readings (known as zero offset calibration). Figure 3 shows the plot of the results. These output values have already been zero-offset compensated.

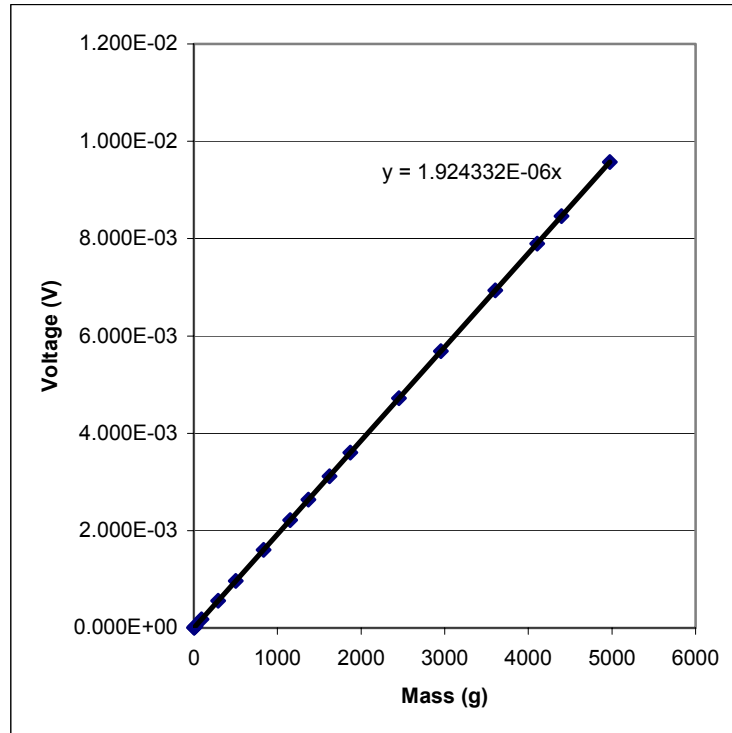


Figure 3. Output Voltage vs. Load

Curve fitting with a straight line produces a line with slope $1.9243\mu\text{V/g}$. As a sanity check, curve fitting using a polynomial curve of degree 2 is also done. This comparison produces the curve:

$$y = -1.40\text{e-}13(x^2) + 1.925\text{e-}6(x).$$

Since the coefficient for the x^2 term is seven orders of magnitude smaller than the x term, the effect of the squared term is insignificant. We conclude the load cell output behavior is linear. The rated output is $(1.9243\mu\text{V/g} * 5000\text{g}) / 5\text{V} = 1.9243 \text{ mV/V}$.

3.4 Calculating the Display Resolution (Count)

The purpose of this section is to develop the theory used in determining the count or flicker of the system shown in Fig. 2. Assuming an external 5V power supply is used as the ADC reference, the PGA is set to 128, and the decimation ratio is 1571, we measured an ENOB of 19.3 bits.

An ENOB of 19.3 bits means 4.7 bits are lost due to undesired noise. In other words, there is $2^{4.7} = 26$ LSB of RMS noise.

$$\text{RMS noise} = 2^{4.7} * 4.67\text{nV} = 121.38\text{nV}$$

This number represents one standard deviation (σ) from the mean of a Gaussian distribution. 66% of the voltage output measurements fall within the interval [mean-121.38nV, mean+121.38nV]. We would like to know the full peak-to-peak noise because that represents the maximum difference (or flicker) that one could see between any two output voltages. This flicker in volts is therefore proportional to the flicker in kilograms. For a Gaussian distribution, over 99% of the readings fall within the interval [mean-3.3 σ , mean+3.3 σ]; thus, over 99% of the readings are distributed over 6.6 standard deviations.

$$\text{Peak-to-peak noise (volts)} = 6.6 * \sigma = 6.6 * \text{RMS noise} = 801.108\text{nV}.$$

Therefore, 801.108nV is the maximum flicker one can observe between any two voltage readings. Next, we must convert the flicker in volts to the flicker in kilograms. From the fundamentals section, we know how to convert the voltage to weight:

$$\text{Mass (kg)} = (\text{observed voltage}) / (\text{rated output} * \text{excitation}) * \text{capacity}$$

So:

$$\begin{aligned} \text{Flicker (kg)} &= (\text{peak-to-peak noise (volts)}) / (\text{rated output} * \text{excitation}) * \text{capacity} \\ &= 801.108\text{nV} / (1.9243\text{mV/V} * 5\text{V}) * 5\text{kg} \\ &= 0.42 \text{ grams} \end{aligned}$$

There should be at most 0.42 grams of flicker between any two readings. The display resolution of the system is half of the flicker, which is +/- 0.21 grams (or 1 count in 25000). For example, if the average of a sample of weight readings is 500g, then there is a confidence level of over 99% that no reading is more than 500.21g and no reading is less than 499.79g.

3.5 Reference Voltage

This section discusses the trade-offs between using an external and internal reference. One of the advantages of using the power supply as the excitation and reference source is that the load cell output and the ADC reference vary ratiometrically as the power supply varies. Noise at the power supply is common to load cell output (or ADC input) and the reference signal. If an internal reference is used, noise at the load cell output (due to noise in the power supply) is no longer common to the reference signal. We can see that noise performance is worse compared to using the power supply as the external reference.

On the other hand, using the internal reference reduces the LSB step size. For example, for a 2.5V reference and a PGA set to 128, the LSB step size is 2.32nV, which is twice as small as using a 5V reference. The decrease in LSB step size might be more than enough to offset the difference in noise performance. To find out which choice is superior over the other, we need to go through the steps outlined in the previous section in order to calculate the resolution of this system (internal reference = 2.5V, PGA = 128). To do that, we need to measure the ENOB of the system under these conditions.

We found the ENOB of the system to be about 18.3 bits (or 1 count in 323000). After performing the steps outlined in the previous section, the display resolution was +/- 0.2grams or 1 count in 25000. This number is almost identical to the set up of figure 2 (external reference = 5V power supply, PGA=128). Thus, neither reference configuration is superior over the other.

When using the 2.5V internal reference, we found that the ENOB performance decreases for heavier loads (that is, when the magnitude of the voltage seen across the ADC inputs increases). When no load was applied, an ENOB of 18.3 bits was observed. When the maximum 5kg load was applied, an ENOB of 17.8 bits (or 1 count in 228000) was observed. As the load increases, then, the amount of noise increases and the internal resolution is no longer four times the display resolution. This behavior was not observed when the power supply was used as the reference. That is, the ENOB remains the same regardless of the magnitude of the load cell output voltage. Since this application note discusses maximizing the precision of the MSC1210, we will use the original configuration (external reference = 5V, PGA = 128) for the remainder of the report.

3.6 Filtering, Display Rate, and Settling Time

Better noise performance can be achieved using software filtering. A simple averaging algorithm can reduce the undesired noise by a factor of (sample size)^{1/2}. For example, if we are to perform averaging over 4 samples (a window size of 4), the noise effectively is reduced by a factor of 2. The trade-off with averaging is speed; we need to wait for 4 samples before a new conversion result is produced. The display update time therefore is increased by a factor of 4. The settling time, which is the time required for a new sample to propagate through the averaging window, is also quadrupled. Thus, a system utilizing software averaging of window size 4 has a settling time of 0.4s (instead of 0.1s with no averaging) and a display rate of 2.5Hz. Modifying the simple averaging algorithm can alleviate the slow display rate problem. Using a running average serves this purpose. The running average can be computed as follows:

$$\text{Ave}(n) = \text{ave}(n-1) + (\text{sample} - \text{ave}(n-1))/N$$

Where ave(n) is the current average, ave(n-1) is the previous average, sample is the current ADC output, and N is the window size.

The running average is therefore a function of the current sample and the averages of the previous samples. Hence, a new average value is produced every time a new ADC output is generated. In other words, the display rate is the same as the data rate. The settling time, however, is independent of the averaging algorithm and can only be reduced by decreasing the window size.

3.7 Dynamically Controlled Window Sizes

Sometimes, it may be preferable to display readings in two steps. First, after a new weight is placed on the scale, a low-resolution reading is quickly displayed. This reading is accurate, but only has a small number of noise-free bits. This event corresponds to using a small averaging window. As time progresses, readings with higher and higher noise-free bits are displayed, corresponding to using bigger and bigger averaging window sizes. To the user, s/he sees digits settling one by one from the lowest resolution to the higher resolution.

In other words, we need to implement a state machine in software that dynamically controls the averaging window sizes. To determine which window size to use, the state machine must monitor successive weight readings. Figure 4 illustrates the operation of the state machine, using a 3-state state machine (S2, S4, and S8) as an example. Each state corresponds to using a window size of 2, 4, and 8 respectively. When a new weight is placed on the load cell initially, the difference between successive readings is larger than some predetermined threshold (thres1). The machine moves into state S2. As the weight begins to settle, the difference between successive readings become smaller and falls below thres1. At this point, the machine shifts into state S4. Finally, when the difference falls below some threshold (thres2, where thres2 < thres1), the machine moves into state S8, and stays there as long as the weight remains on the load cell.

Suppose a different weight is now placed on the load cell. The difference initially becomes so large that it exceeds thres1. The machine shifts back to state S2, but eventually the machine will settle back into state S8 through state S4 (as long as the weight remains on the load cell).

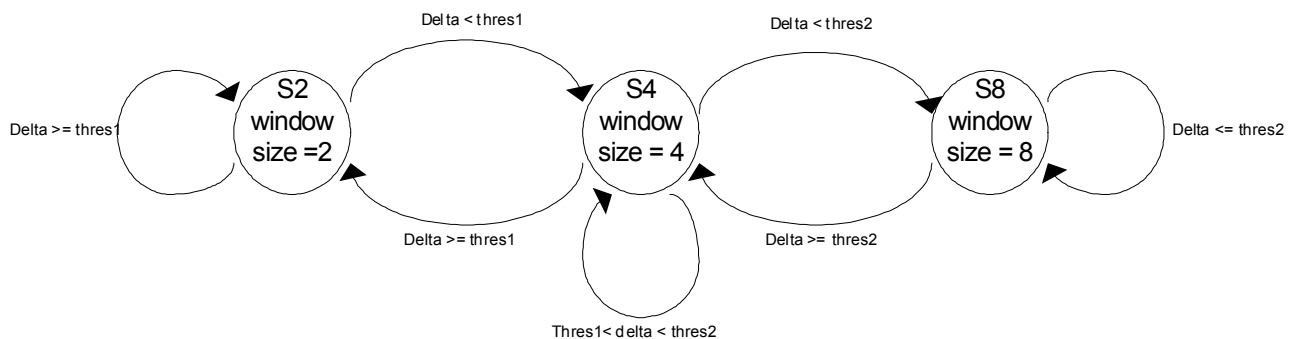


Figure 4. Example of State Machine for Dynamically Controlling Window Sizes

3.8 Temperature Drift Compensation

Temperature drift occurs in most weight scale applications because of changes in the ambient environment or because of self-heating that occurs when the bridge resistors are excited. If the load cell experiences any temperature change, it expands and induces a strain in the bridge resistors, even when no force is applied. Therefore, it is desirable to perform an offset calibration to compensate the effect caused by temperature drift when the temperature changes by more than a specified amount (even by a few degrees).

We can use the temperature sensor that is built into the MSC1210 to monitor the temperature of the environment. At the end of each offset calibration, the temperature sensor voltage is measured. This output is then converted to a temperature reading using two-point extrapolation. According to the MSC1210 datasheet, the temperature sensor voltage is 115mV at 25 degrees Celsius and the sensor coefficient is 375 $\mu\text{V}/\text{C}$. To convert the voltage to temperature, we just perform an extrapolation of a straight line based on these two parameters. A monitor program can be set up such that at specified intervals the temperature sensor voltage is measured and converted to a temperature reading. If the current temperature differs from the post-offset calibration reading by more than a specified amount, we perform another offset calibration.

4 Results

The measurements discussed in this section are taken under the following configuration:

MSC1210 set up

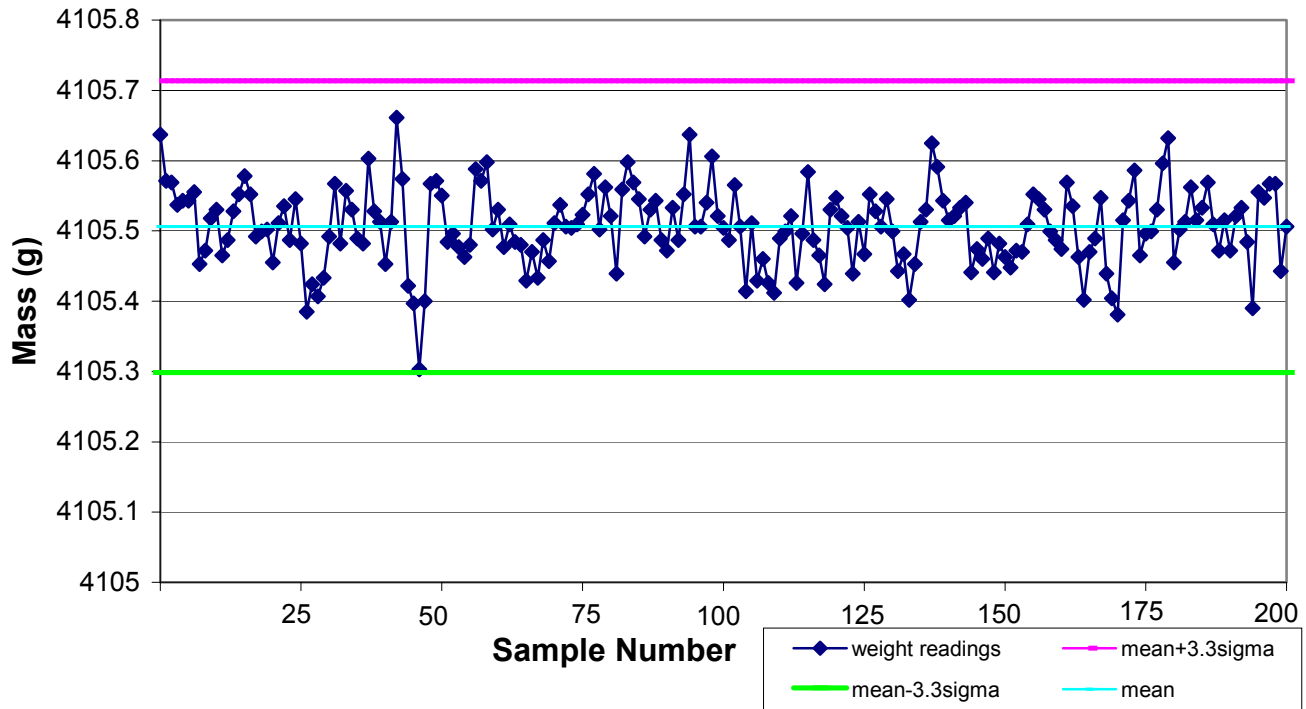
- External crystal frequency: 11.0592 MHz
- ACLK register = 10
- Decimation ratio = 1571 (or equivalently 10Hz)
- Buffer off
- PGA = 128
- External reference = 5V
- Offset DAC = 0
- Bipolar inputs
- System offset calibration only

Load cell parameters

- Rated output: 1.92293 mV/V
- Excitation: 5V (minimum recommended voltage)
- Capacity: 5kg

4.1 No Averaging

A 4105.5 gram weight is placed on the load cell and 200 consecutive weight readings are recorded. The following figure is a plot of the results.



**Figure 5. 200 Consecutive Readings
(mean = 4105.506g, ENOB = 19.3)**

The ENOB for these 200 samples is 19.3. This translates to a peak-to-peak noise of 799.83nV and a flicker of 0.42g. The display resolution is therefore +/- 0.21g (or 1 count in 25000). These numbers are consistent with those calculated in Section 3.

The middle horizontal line is the mean of these 200 measurements. The top horizontal line is the upper limit; that is, there is a confidence level of over 99% that no reading is more than $4105.506 + 0.21\text{g}$. The bottom horizontal line is the lower limit; that is, there is a confidence level of over 99% that no reading is less than $4105.506 - 0.21\text{g}$. The above figure confirms that out of these 200 measurements, all of them fall within the upper and lower limits.

Figure 6 is a histogram plot of the same data in Figure 5 (bin width = 0.0358g).

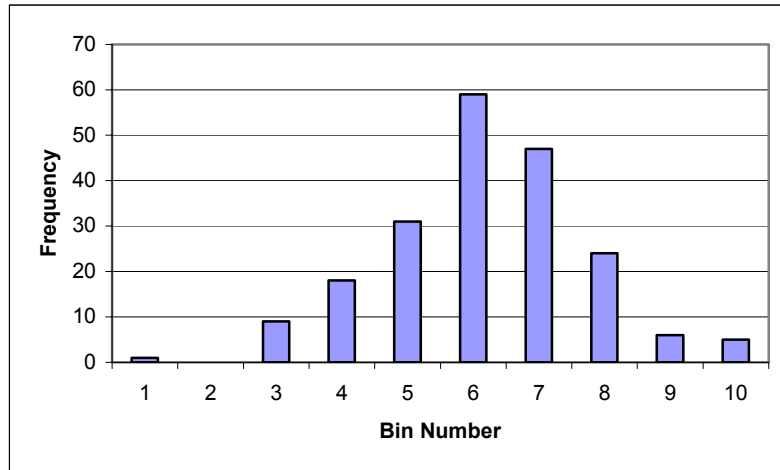


Figure 6. Histogram for Data in Figure 5

The maximum value is 4105.661g and the minimum value is 4105.303g. These 200 samples are distributed over 10 bins. The bin width is $(4105.661 - 4105.303)/10 = 0.0358\text{g}$. The intervals for each bin are listed in the Table 1.

Table 1. Bin Number and Interval

Bin Number	Interval (g)
1	4105.303 – 4105.339
2	4105.339 – 4105.375
3	4105.375 – 4105.410
4	4105.410 – 4105.446
5	4105.446 – 4105.482
6	4105.482 – 4105.518
7	4105.518 – 4105.554
8	4105.554 – 4105.589
9	4105.589 – 4105.625
10	4105.625 – 4105.661

The average value is located in bin 6.

4.2 Running Average

The following plot shows 200 weight readings, using a running average of window size 8.

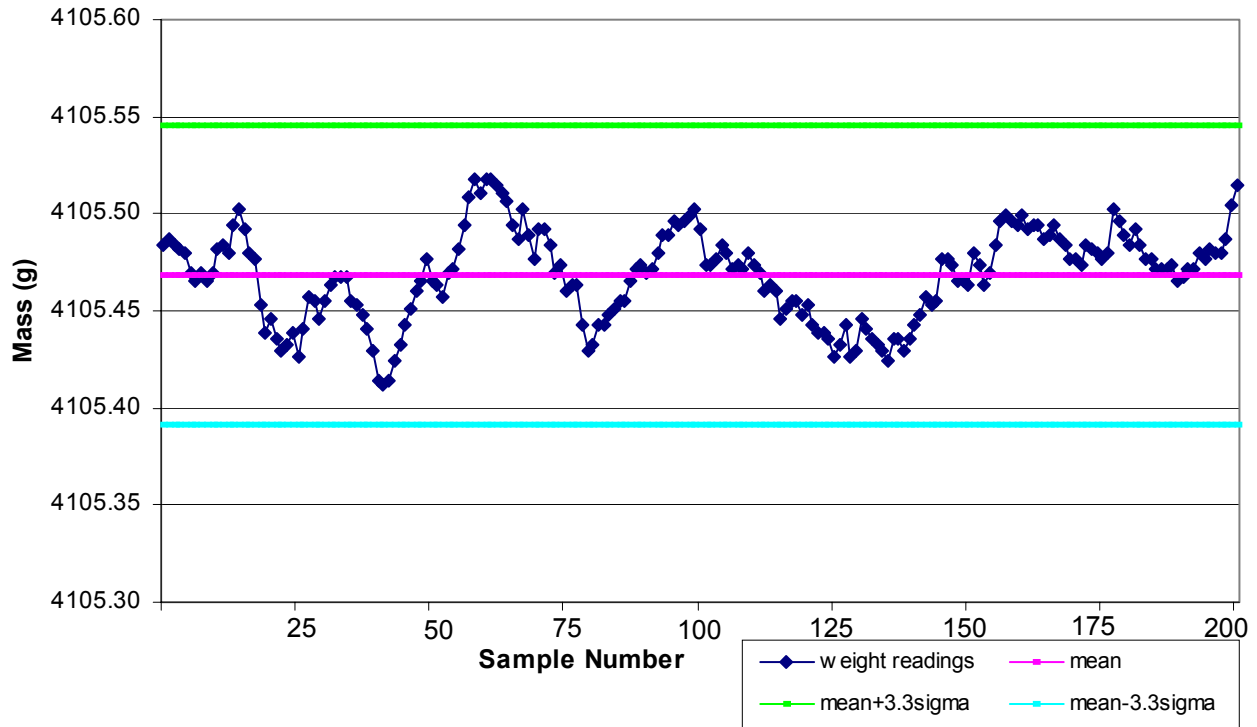


Figure 7. 200 Consecutive Readings, Window Size = 8
(mean = 4105.469g, ENOB = 20.7)

The ENOB for these 200 samples is 20.7. This translates to a peak-to-peak noise of 296.38nV and a flicker of 0.15g. The display resolution is therefore +/- 0.08g (or 1 count in 62500). The middle horizontal line is the mean of these 200 measurements. The top horizontal line is the upper limit, and the bottom horizontal line is the lower limit. We expect the data show that there is a confidence level of over 99% that no reading is more than 4105.469+0.08g or less than 4105.469-0.08g. Fig. 7 confirms that out of these 200 measurements, all of them fall within the upper and lower limits.

Figure 8 is a histogram plot of the same data in Figure 7 (bin width = 0.01g).

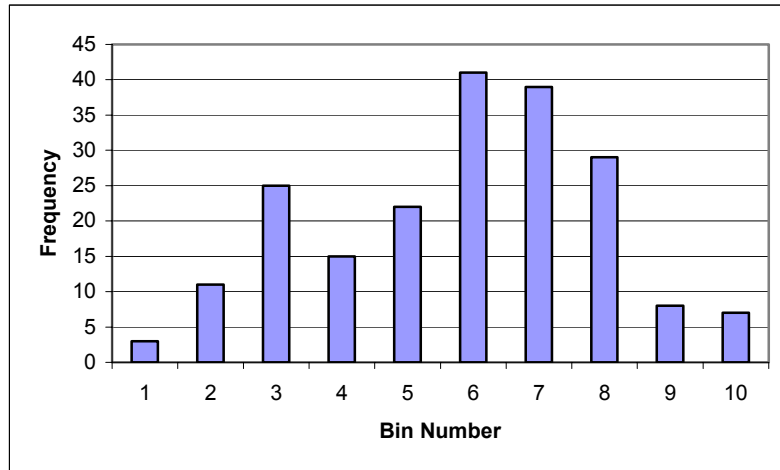


Figure 8. Histogram for Data in Figure 7

The maximum value is 4105.518g and the minimum value is 4105.412g. These 200 samples are distributed over 10 bins. The bin width is $(4105.518 - 4105.412)/10 = 0.01g$. The intervals for each bin are listed in Table 2.

Table 2. Bin Number and Interval

Bin Number	Interval (g)
1	4105.412 – 4105.423
2	4105.423 – 4105.433
3	4105.433 – 4105.444
4	4105.444 – 4105.454
5	4105.454 – 4105.465
6	4105.465 – 4105.476
7	4105.476 – 4105.486
8	4105.486 – 4105.497
9	4105.497 – 4105.507
10	4105.507 – 4105.518

The average value is located in bin 6.

5 Summary

The results of the two tests are summarized in Table 3. By averaging over 8 samples, we effectively increased the resolution of the weight scale by a factor greater than 2. The settling time, however, is increased 8 times, to approximately 1s. We feel this trade-off is acceptable in weight scale applications because most users do not need to apply a different weight on the scale every second.

Table 3. Summary of Results

Parameter	No Averaging	Moving Average
LSB	4.67nV	4.67nV
ENOB	19.3 bits	20.7 bits
RMS noise (one standard deviation)	121.38nV	44.75nV
Peak-to-peak noise (6.6 standard deviation)	801.108nV	295.38nV
Flicker	0.42g	0.15g
Display Resolution	+/- 0.21g	+/- 0.08g
Count	1 in 25000	1 in 62500

Example Code

In this section, we include the sample C program ***conv.c*** and assembly program ***adc_sub.a51***. The latter file contains subroutines, which are called out by the C program. This sample program generates the results that are presented in the previous section. A listing file is also included to give the user an estimate of the code and data size.


```

//conv.c
#include "MSC1210.H"
#include <stdio.h>
#include <stdlib.h>
#include <math.h>
extern void autobaud(void);
extern unsigned long unipolar(void);
extern unsigned long bipolar(void);
extern signed long deltasigma(void);
extern signed long adc_win(unsigned char);
extern char rx_byte(void);
extern void putcr(void);
#define rated_output 1.92433e-3
#define capacity 5000
#define excitation 5

void adc_mave(unsigned int n, float k, float conv_factor)
{
    unsigned char xdata *winptr;
    long int idata adcsun;
    long int sw_offset_mave=0;
    unsigned int fill_ptr=1, mod_ptr=0 ;
    adcsun=0; deltasigma(); // dispose one conversion
    //acquire the sw offset,
    sw_offset_mave = deltasigma();
    printf(" Volts\t \t grams\n");
    while (RI==0) {
        adcsun=adcsun+adc_win(mod_ptr);
        printf("%1.8f\t %f\n", (float)((adcsun / fill_ptr)-
sw_offset_mave)*k, (float)((adcsun / fill_ptr)-sw_offset_mave)*k*conv_factor);
        if (fill_ptr==n) fill_ptr=n; else fill_ptr++;
        if (mod_ptr==(n-1)) mod_ptr=0; else mod_ptr++;
    }
    rx_byte(); // Flush serial byte
}

void main(void)
{
    signed long int xdata adres[200];
    signed long int dummy;
    signed long int sw_offset;
    int i;
    int j;
    char s;
    float ave,sd,n,k, conv_factor;
    CKCON &= 0xf8; // 0 MOVX cycle stretch
    k = 5/(pow(2,23)*128); //1 LSB in volts
    //Timer Setup
    ONEUSEC= 10; // 11.0592MHz Clock !!!!!
    ONEMSL=0x32;
    ONEMSH=0x2B;
    HUNDMS=0x63;
    PWRMGT &= 0xf7; //turn on adc

    autobaud(); RI=0;
    printf("MSC1210 load cell Test\n");
    printf("1) Acquire 200 samples and perform stats analysis\n");
    printf("2) Moving average dump\n");
    scanf("%c",&s);
}

```

```

/* Setup ADC */
P1DDRH |= 0xc0;
ADCLK = 10; //11.0592MHz => modclk = 15.6kHz
ADMUX = 0x067; // Select AIN6-AIN7
ADCON0 = 0x07; // Vref off , Buff off, BOD off, PGA=128
ADCON1 = 0x00; // bipolar
ADCON2 = 0x23; // decimation ratio = 1571 => data rate = 10Hz
ADCON3 = 0x06;
ADCON1 = 0x04; // bipolar, auto, system calibration, offset
PGASHFT = 0;
//wait for the calibration to take place
printf ("\n\n System Calibrating...\n");
for (i=0;i<5;i++){ // dump 5 conversions
    while(!(PIREG & 0x20)){
        dummy=bipolar();
    }
while(!(PIREG & 0x20)){
    sw_offset=bipolar(); //get the zero load offset after calibration
if (s=='1') { //s=='1'
    ADMUX = 0x67; //AIN6-AIN7
    conv_factor = capacity/(rated_output*excitation);
    while (1){
        printf("voltage -> mass(g)\n");
        for (i=0;i<200;i++){ // acquire 200 points
            while(!(PIREG & 0x20)){
                adres[i]=bipolar()-sw_offset;
//subtract zero load offset from reading
                printf ("%1.8f\t %f\n",
(float)adres[i]*k, (float)adres[i]*k*conv_factor);
            }
            ave=0; n=0; sd=0; j=0;
            for (i=0;i<200;i++){
                ave+= adres[i]; n++;
            }
            ave= ave/n;
            for (i=0;i<200;i++){
                sd += pow(adres[i]-ave,2);
            }
            sd= sqrt(sd/n);
            printf("\n**** In LSB:
SD=%3.2f\tMean(volts)=%1.8f\tN=%4d\tENOB=%3.2F****\n",sd,ave*k, (int)n, 24-
log(sd)/log(2));
        } //while(1)
    } //if s=='1'
    else {
        adc_mave(8,k, conv_factor);
    } // else
} // main

```

```

//adc_sub.a51
$NOMOD51
#include (reg1210.inc)
PUBLIC unipolar, bipolar, read_sum_regs
PUBLIC deltasigma, _adc_win
adc_sub      SEGMENT  CODE
             RSEG   adc_sub

;;;;;;;;;;;;;
; moving average ADC conversion and window calc
; long int adc_win(unsigned char i);
; return adc - win[i] and update win[i] with adc
; i point to long int xdata array
_adc_win:
    mov     a, r7           ; r7*4-> DPTR
    swap   a               ; r7.7~6 -> dph.1~0
    rr     a
    rr     a
    anl    a,#03h
    mov    dph,a
    mov    a,r7           ; r7.5~0,0,0 -> dpl
    rl     a
    rl     a
    anl    a,#0fch
    mov    dpl,a
    call   deltasigma     ; adc -> r4~7
    movx   a,@dptr       ; r0~3 <- win[i], win[i] <- adc
    mov    r0,a
    mov    a, r4
    movx   @dptr,a
    inc   dptr
    movx   a,@dptr
    mov    r1,a
    mov    a, r5
    movx   @dptr,a
    inc   dptr
    movx   a,@dptr
    mov    r2,a
    mov    a, r6
    movx   @dptr,a
    inc   dptr
    movx   a,@dptr
    mov    r3,a
    mov    a, r7
    movx   @dptr,a
adcsb:
    clr    c              ; r4~7 <- r4~7(adc) - r0~3 (old win[i])
    mov    a,r7
    subb   a,r3
    mov    r7,a
    mov    a,r6
    subb   a,r2
    mov    r6,a
    mov    a,r5
    subb   a,r1
    mov    r5,a
    mov    a,r4
    subb   a,r0
    mov    r4,a
    ret

```

```

;;;;;;;;;;;;;
; signed long deltasigma(void)
; return the 3 byte adres to R4567 (MSB~LSB)
; return signed long int with sign-extend R4 for bipolar
; and stuff 0 on R4 for unipolar
; ADCON0[7]=OSE
;P1.7 =0: Conversion with reversed ADMUX
;
;          +----- reverse ADMUX (Last-ADC)/2
;          | +----- default ADMUX
;          | | +---- (ADC-Last)/2
;          V  V  V
;P1.7 -----|-----|-----|-----
;
;
;
;
deltasigma:
    mov     a,ADCON0
    rlc     a
    jnc     ds_once      ; if AZ=0 then ds once
    jb     P1.7, ds_nosw ; default ADMUX setting
    mov     a,ADMUX
    swap    a
    mov     ADMUX,a
ds_nosw:
    call    ds_once
    call    ds_once
    call    ds_once
    call    ds_once
    call    ds_once      ; r4~7 <- new adc
    mov     r3,DPL1      ; r0~3 <- last adc
    mov     r2,DPH1
    mov     r1,BPL
    mov     r0,BPH
    mov     DPL1,r7      ; last <- new
    mov     DPH1,r6
    mov     BPL,r5
    mov     BPH,r4
    jb     P1.7,ds_adcsb ; If set: (ADC-Last)/2 else (Last-ADC)/2
    mov     a,r7          ; XCH (r4~7, r0~3)
    xch     a,r3
    xch     a,r7
    mov     a,r6
    xch     a,r2
    xch     a,r6
    mov     a,r5
    xch     a,r1
    xch     a,r5
    mov     a,r4
    xch     a,r0
    xch     a,r4
ds_adcsb:
    call    adcsb        ; adcsb: r4~7 -= r0~3 ;
    mov     a,r4          ; r4~7 /= 2; 2's comp div
    rlc     a              ; c has sign
    mov     a,r4          ; (c,r4)>>1->c
    rrc     a
    mov     r4,a
    mov     a,r5          ; (c,r5)>>1->c
    rrc     a

```

```

        mov     r5,a
        mov     a,r6           ;   (c,r6)>>1->c
        rrc     a
        mov     r6,a
        mov     a,r7           ;   (c,r7)>>1->c
        rrc     a
        mov     r7,a
        jb      P1.7, ds_done
        mov     a,ADMUX
        swap    a
        mov     ADMUX,a
ds_done:
        cpl     P1.7
        ret
ds_once:
        mov     a,AIE
        jnb     acc.5,ds_once
        mov     r4,#0
        mov     r5,adresh
        mov     r6,adresm
        mov     r7,adresl
        mov     a,ADCON1
        jb      acc.6, ds_unipolar           ; stuffed zero for unipolar
        mov     a,r5
        jnb     acc.7,ds_positive           ; sign-extend for bipolar
        mov     r4,#0ffh
ds_positive:
ds_unipolar:
        cpl     P1.4
        ret

;;;;;;;;;;;;;
; unsigned long unipolar(void)
; return the 3 byte adres to R4567 (MSB~LSB)
; unsigned long int with R4=0
unipolar:
        mov     r4,#0
        mov     r5,adresh
        mov     r6,adresm
        mov     r7,adresl
        ret

;;;;;;;;;;;;;
; signed long bipolar(void)
; return the 3 byte adres to R4567 (MSB~LSB)
; return signed long int with sign extension on R4
bipolar:
        mov     r4,#0
        mov     a,adresh
        mov     r5,a
        mov     r6,adresm
        mov     r7,adresl
        jnb     acc.7,positive
        mov     r4,#0ffh
positive:
        ret

;;;;;;;;;;;;;
; signed long read_sum_regs(void)
; return the 4 byte sumr to R4567 (MSB~LSB)
; return signed long int, sign extension done by hardware
read_sum_regs:

```

```
mov     r4, SUMR3;
mov     r5, SUMR2;
mov     r6, SUMR1;
mov     r7, SUMR0;
ret
end
```

```
//conv.lst
...
<snip>
...
MODULE INFORMATION:   STATIC OVERLAYABLE
  CODE SIZE           =    1158   ----
  CONSTANT SIZE       =     240   ----
  XDATA SIZE          =     ----   851
  PDATA SIZE          =     ----   ----
  DATA SIZE          =     ----   ----
  IDATA SIZE          =     ----    4
  BIT SIZE            =     ----   ----
END OF MODULE INFORMATION.

C51 COMPILATION COMPLETE.  0 WARNING(S),  0 ERROR(S)
```

References

1. *MSC1210Yx Datasheet (SBAS203A)*

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